

There are 5 reactions and 4 species in the OMM model.

The stoichiometric matrix is $S =$

$$\begin{matrix} -1 & 1 & 1 & 0 & 0 \\ -1 & 1 & 0 & 1 & 0 \\ 1 & -1 & -1 & 0 & 0 \\ 0 & 0 & 1 & 0 & -1 \end{matrix}$$

The vector of reaction velocities is v , where

$$\begin{aligned} v(1) &= k_1 * x_1 * x_2 \\ v(2) &= k_2 * x_3 \\ v(3) &= k_3 * x_3 \\ v(4) &= k_4 \\ v(5) &= k_5 * x_4 \end{aligned}$$

The vector of mass balance equations is $x_{dot} = S*v$, where

$$\begin{aligned} x_{dot}(1) &= k_2 * x_3 + k_3 * x_3 - k_1 * x_1 * x_2 \\ x_{dot}(2) &= k_4 + k_2 * x_3 - k_1 * x_1 * x_2 \\ x_{dot}(3) &= k_1 * x_1 * x_2 - k_3 * x_3 - k_2 * x_3 \\ x_{dot}(4) &= k_3 * x_3 - k_5 * x_4 \end{aligned}$$

Let the map ψ_p be given by

$$\begin{array}{l|l} \begin{matrix} k_1 \\ k_2 \\ k_3 \\ k_4 \\ k_5 \\ x_1 \\ x_2 \\ x_3 \\ x_4 \end{matrix} & \begin{matrix} \rightarrow y_1 \\ \rightarrow y_2 \\ \rightarrow y_3 \\ \rightarrow y_4 \\ \rightarrow y_5 \\ \rightarrow p_1 \\ \rightarrow p_2 \\ \rightarrow p_3 \\ \rightarrow p_4 \end{matrix} \end{array}$$

This results in a linear velocity vector $\psi_p(v)$, where

$$\begin{aligned} \psi_p(v(1)) &= p_1 * p_2 * y_1 \\ \psi_p(v(2)) &= p_3 * y_2 \\ \psi_p(v(3)) &= p_3 * y_3 \\ \psi_p(v(4)) &= y_4 \\ \psi_p(v(5)) &= p_4 * y_5 \end{aligned}$$

We can express $\psi_p(v)$ as the product $P*y$, where y is the vector $[y_1, \dots, y_5]^T$ and $P =$

$$\begin{matrix} p_1 * p_2 & 0 & 0 & 0 & 0 \\ 0 & p_3 & 0 & 0 & 0 \\ 0 & 0 & p_3 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & p_4 \end{matrix}$$

From this we calculate the coefficient matrix, $C = S*P =$

$$\begin{matrix} -p_1 * p_2 & p_3 & p_3 & 0 & 0 \\ -p_1 * p_2 & p_3 & 0 & 1 & 0 \\ p_1 * p_2 & -p_3 & -p_3 & 0 & 0 \\ 0 & 0 & p_3 & 0 & -p_4 \end{matrix}$$

C is row equivalent to the reduced matrix $Crref =$

$$\begin{matrix} 1 & -p_3 / (p_1 * p_2) & 0 & 0 & -p_4 / (p_1 * p_2) \\ 0 & 0 & 1 & 0 & -p_4 / p_3 \\ 0 & 0 & 0 & 1 & -p_4 \\ 0 & 0 & 0 & 0 & 0 \end{matrix}$$

The null space of C is spanned by the columns of N =

$$\begin{matrix} p_3/(p_1*p_2) & p_4/(p_1*p_2) \\ 1 & 0 \\ 0 & p_4/p_3 \\ 0 & p_4 \\ 0 & 1 \end{matrix}$$

Let $ybar = N*q$, where q is given by

$$\begin{matrix} q(1) = q_1 \\ q(2) = q_2 \end{matrix}$$

This gives

$$\begin{matrix} ybar(1) = (p_3*q_1 + p_4*q_2)/(p_1*p_2) \\ ybar(2) = q_1 \\ ybar(3) = (p_4*q_2)/p_3 \\ ybar(4) = p_4*q_2 \\ ybar(5) = q_2 \end{matrix}$$

From ybar we construct the composite forward map psi_py :

$$\begin{matrix} k_1 \rightarrow (p_3*q_1 + p_4*q_2)/(p_1*p_2) \\ k_2 \rightarrow q_1 \\ k_3 \rightarrow (p_4*q_2)/p_3 \\ k_4 \rightarrow p_4*q_2 \\ k_5 \rightarrow q_2 \\ x_1 \rightarrow p_1 \\ x_2 \rightarrow p_2 \\ x_3 \rightarrow p_3 \\ x_4 \rightarrow p_4 \end{matrix}$$

The steady state reaction velocity vector vbar is given by psi_py(v), where

$$\begin{matrix} vbar(1) = p_3*q_1 + p_4*q_2 \\ vbar(2) = p_3*q_1 \\ vbar(3) = p_4*q_2 \\ vbar(4) = p_4*q_2 \\ vbar(5) = p_4*q_2 \end{matrix}$$

The mapping function psi_q^-1 is given by

$$\begin{matrix} q_1 \rightarrow y_2 \\ q_2 \rightarrow y_5 \end{matrix}$$

The composite inverse map psi_qp^-1:

$$\begin{matrix} p_1 \rightarrow x_1 \\ p_2 \rightarrow x_2 \\ p_3 \rightarrow x_3 \\ p_4 \rightarrow x_4 \\ q_1 \rightarrow k_2 \\ q_2 \rightarrow k_5 \end{matrix}$$

The complete steady state map psi_ss is therefore

$$\begin{matrix} k_1 \rightarrow (k_2*x_3 + k_5*x_4)/(x_1*x_2) \\ k_2 \rightarrow k_2 \\ k_3 \rightarrow (k_5*x_4)/x_3 \\ k_4 \rightarrow k_5*x_4 \\ k_5 \rightarrow k_5 \\ x_1 \rightarrow x_1 \\ x_2 \rightarrow x_2 \\ x_3 \rightarrow x_3 \\ x_4 \rightarrow x_4 \end{matrix}$$

The unsubstituted steady state reaction velocity vector vbar = psi_ss(v) is

given by

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vbar(1) = k2*x3 + k5*x4
vbar(2) = k2*x3
vbar(3) = k5*x4
vbar(4) = k5*x4
vbar(5) = k5*x4
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Verify steady state. $\dot{x} = S * vbar$, where

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xdot(1) = 0
xdot(2) = 0
xdot(3) = 0
xdot(4) = 0
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